Separation of Random Telegraph Signals from $1/f$ Noise in MOSFETs under Constant and Switched Bias Conditions

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Abstract

The low-frequency noise power spectrum of small dimension MOSFETs is dominated by Lorentzians arising from Random Telegraph Signals (RTS). The low-frequency noise is observed to decrease when the devices are periodically switched ‘off’. The technique of determining the statistical lifetimes and amplitudes of the RTS by fitting the signal level histogram of the time-domain record to two-Gaussian histograms has been reported in literature. This procedure is then used for analysing the ‘noisy’ RTS along with the device background noise, which turned out to be $1/f$ noise. The $1/f$ noise of the device can then be separated from the RTS using this procedure. In this work, RTS observed in MOSFETs, under both constant and switched biased conditions, have been investigated in the time domain. Further, the $1/f$ noise in both the constant and the switched biased conditions is investigated.

1. Introduction

The low-frequency noise is very important for analog and RF applications in advanced CMOS technologies. As device dimensions shrink the low-frequency noise increases. In such devices, the low-frequency noise performance is dominated by Random Telegraph Signals (RTS) on top of the $1/f$ noise. The origin of such an RTS is attributed to the random trapping and de-trapping of mobile charge carriers in traps located in the oxide or at the interface. An RTS has two distinct levels and it switches between the two states at random moments. The RTS is observed in MOSFETs as a fluctuation in the drain current. The most common way of an RTS analysis is measuring the averaged power spectral density in the frequency domain. A pure two-level RTS is represented in the frequency domain by a Lorentzian spectrum [1]. However, the spectral means do not provide us with complete information about the RTS. The spectral measurements provide only the value of the corner frequency, the frequency above which the spectral density rolls off as $f^{-2}$ and does not give the average lifetimes in the individual states, but only the harmonic mean of these two characteristic time constants. A time domain measurement can be useful in extracting all the RTS parameters. The standard procedure for the analysis of RTS in time domain consists of directly finding from the time record the time instances at which the signal is in the distinct state. Using a simple level-crossing algorithm one can then determine the instances of the ‘high’ and ‘low’ states of the RTS. This simple procedure can be used effectively for a clean RTS, where the ratio of the RTS amplitude to background noise is high. Another procedure for analysing RTS in the time domain is based on the analysis of the signal level histogram of the measured signal and the separation of the data points into two records each corresponding to one of the RTS levels [2]. Using this procedure it is possible to separate out the RTS from the background noise.

The RTS noise decreases when the gate bias is periodically alternated between an ‘on’ state where the device is in strong inversion and saturation and an ‘off’ state where the $V_{GS}$ (gate-to-source voltage) is well below the threshold voltage of the device [3-6].

In this paper, we analyse the RTS observed in p-MOSFETs, under constant and switched biased (cyclo-stationary) conditions. The time domain procedure in [2] is then used to separate the RTS from the background noise under both conditions.

2. RTS measurement in time domain

2.1. Measurement Setup

The measurement setup used for the noise measurements is the same as that used in [6]. A digital oscilloscope (TDS7404) is used for recording the time domain RTS data. Large time frames of the RTS are obtained in an automated manner using LabVIEW and TekVISA. Under ‘switched bias’ conditions the device is periodically switched ‘off’, by applying a square wave with a 50% duty cycle at the gate of the device. The switching frequency is much higher than the RTS corner frequency. The ‘switched biased’ output is then sampled only in the ‘on’ state of the MOSFET. These ‘on’ states are then joined together to form a ‘switched biased’ RTS.

Figure 1 shows a schematic of the ‘switched biased’ RTS. The measurement setup [6], along with an RTS parameter extraction procedure [7], can be used...
successfully to extract the RTS parameters under constant and switched bias conditions. The extracted parameters are then used in Machlup’s analytical noise-power expression [1], and compared with the noise power measured using a spectrum analyser.

3. RTS measurement results

The devices under test are p-channel MOSFETs, with a W/L=10/0.3 (µm), with a gate oxide thickness of 10nm.

The setup measures the drain current noise power spectral density (PSD) of the device under test (dB V²/Hz). Figure 3 shows a sample of a time-domain RTS obtained from the drain current measurement of a device under constant bias.
The first step of the noise separation procedure is shown in Fig. 4 for a device under constant bias. Figure 4 shows two distinct peaks each corresponding to the RTS level surrounded by the device background noise with a Gaussian distribution. The data points are then grouped into two levels. The RTS amplitude (difference between the two Gaussian peaks) is then subtracted from the ‘high’ level to give the device background noise data.

The PSD of the device background noise is then calculated. Figure 5 shows the PSD of an RTS measured under constant bias conditions using a spectrum analyzer. Also shown is the PSD of the device background noise extracted using the above procedure. A line with a slope of $1/f$ (10dB/decade) is then fitted to the PSD of the device background noise. From Fig. 5, it can be seen that the slope of the noise is $1/f$.

The Hooge parameter for the extracted $1/f$ noise was then calculated to be $\alpha_H = 6.8 \times 10^{-6}$.

The same device is then periodically switched ‘off’ with a frequency of 10 kHz and a 50% duty cycle. The switched biased RTS time domain data is obtained using the technique in Fig. 1. Similar to the constant bias case, the signal level histogram is then plotted for the switched biased case. This is shown in Fig. 6. The method for the separation of the background noise in the switched bias case is the same as that for the constant bias case.

The PSD of the device background noise for the switched bias case is also computed. Figure 7 shows the measured PSD of an RTS on a p-MOSFET under switched bias conditions. Also shown are the calculated PSD of the switched biased RTS, and the device $1/f$ noise.

The calculated PSD of the switched biased RTS is higher than the measured PSD. This is because the switched biased RTS is obtained only by sampling the ‘on’ states of device. The measured PSD, on the other hand is got
by sampling both the ‘on’ and ‘off’ states of the device. The PSD of the device background noise under switched bias conditions is also fitted with a line of slope $1/f$ (10dB/decade) From Fig. 7 it can be seen that the device background noise for the switched bias case is also $1/f$ in nature.

4. Discussions

The results of the time domain separation method verify the assumption of the dominating two-level RTS on top of the $1/f$ noise in MOSFETs. Also the PSD of the device background noise is $1/f$ in nature for both the constant and switched bias conditions. The extracted Hooge parameter $\alpha_H=6.8 \times 10^{-6}$, for the device under constant bias conditions, is quite a normal value for these type of devices [9]. Our results show that the time domain analysis of an RTS is not only useful in extracting the RTS parameters, but also in extracting the $1/f$ noise of the device using the separation procedure.

5. Conclusions

Time domain analysis of RTS observed in MOSFETs, under constant and switched biased (cyclo-stationary) conditions has been presented. The time-domain procedure in [2] has been used to separate out the two-level RTS from the device background noise under both conditions. Measurement results indicate that this noise is $1/f$ in nature ($\alpha_H=6.8 \times 10^{-6}$).

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References